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Stein estimation in the Conway-Maxwell Poisson model with correlated regressors



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ABSTRACT

The Poisson regression model (PRM) is widely used for count data, applicable when the response variable follows a Poisson distribution with equal dispersion. The Conway-Maxwell Poisson regression model (COMPRM) is more flexible and can handle both under-dispersion and over-dispersion. However, the COMPRM may involve correlated regressors, leading to multicollinearity, which makes the maximum likelihood estimator (MLE) inefficient. Biased estimation methods can address multicollinearity in data. This study proposes a Stein estimator, a biased estimation method, for the COMPRM that can simultaneously address correlated regressors and dispersion issues. The estimated mean square error (EMSE) is used to evaluate performance. The proposed estimator's performance is assessed both theoretically and numerically. The numerical evaluations include a simulation study under various parametric conditions and a real-world application. The results from both the simulation study and the real application demonstrate that the Stein estimator outperforms the MLE.

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1. Introduction

Count data models are widely used for counting responses. One of the most popular models is the Poisson model. The Poisson model works with a single parameter as the mean and variance are equal. This property reduces its application and is unable to explain the dispersion problem. Different models are proposed to handle dispersion. Examples include the negative binomial model (Hilbe, 2011), the bell regression model (Majid et al., 2022), and the Poisson mixture, which are used for over-dispersed data and cannot handle underdispersion cases (McLachlan, 1997). A Conway-Maxwell Poisson regression model (COMPRM) can capture both over and under-dispersion for modeling queuing systems with state-dependent service rates introduced by Conwaay and Maxwell (1962).

Moreover, the count data models may be with correlated regressors. In this situation, the maximum likelihood estimator (MLE) provides an inefficient regression coefficient estimate. To address the issue

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of correlated regressors, Stein proposed the Stein estimator (SE) for the LRM (Stein, 1960). Stein estimator is proposed for the logistic regression model. In his study, he presented three biased estimators, ridge, Stein, and principal component regression, and compared them using a Monte Carlo simulation study, but no theoretical comparison is provided (Schaefer, 1986). For the Inverse Gaussian Regression Model, SE performs as an efficient proposed estimator (Akram et al., 2021).

The SE for the logistic regression was proposed by Schaefer (1986). The SE for the Poisson regression model as a case of count data model deals with correlated regressors and equal dispersion by Amin et al. (2022). Akram et al. (2021) considered the SE for the inverse Gaussian regression model. Recently, the SE was adapted for the beta regression model (Amin et al., 2023a). The response variable might be in count form with overdispersion, underdispersion, and correlated regressors. Therefore, we need a biased estimator for the COMPRM. We are considering using the SE as a biased estimator to address the issue of correlated regressors in the COMPRM. Although some researchers have studied this biased estimator, there is no study specifically on using the SE for the COMPRM to address correlated regressors. Thus, we propose a new estimator, the COMP Stein Estimator (COMPSE), to reduce the impact of correlated regressors. The remainder of this study is organized

as follows: Section 2 introduces the COMPRM model and its estimation methods. Additionally, we explain COMPRM and COMPSE along with their MSEs and provide a theoretical comparison of the proposed estimator with the Maximum Likelihood Estimator (MLE). In Section 3, we assess the performance of the estimator using a Monte Carlo simulation. Section 4 involves the application of the model to real data. The final section summarizes the conclusions of the study.

2. Methodology

2.1. The COMP regression model

The COMP distribution is flexible enough to handle the dispersion in count data with an additional parameter (ν) and deals with both overdispersion ($\nu < 1$) and under dispersion ($\nu > 1$). The COMP distribution is the generalization of some well-known discrete distributions. When $\nu =1$, then the COMP distribution approaches the Poisson distribution, when $\nu =0$ and $\lambda < 1$, the COMP distribution is converted to Geometric distribution, and when $\nu \rightarrow \infty$, the COMP distribution approaches the Bernoulli distribution with probability $\left(\frac{\lambda}{1+\lambda}\right)$. Suppose y is a random variable and follows a COMP (λ, ν) with a probability mass function as

$$P(Y = y; \lambda, \nu) = \frac{1}{Z(\lambda, \nu)} \frac{\lambda^y}{(y!)^{\nu'}} \quad y = 0, 1, 2, \dots, \infty$$
(1)

where, $Z(\lambda, \nu) = \sum_{n=0}^{\infty} \frac{\lambda^n}{(n!)^{\nu}}$ is the normalizing constant, λ is the mean parameter, and ν ($\nu > 0$) is the dispersion parameter (Chatla and Shmueli, 2018). The mean and variance of the COMP distribution using an asymptotic expression for Z in Eq. 1 are, respectively (Shmueli et al., 2005).

$$E(Y) \approx \lambda^{\frac{1}{\nu}} + \frac{1}{2\nu} - \frac{1}{2'},$$

$$Var(Y) \approx \frac{1}{\nu} \lambda^{\frac{1}{\nu}}$$
(2)

The reparametrized COMP function is obtained by setting $\mu = \lambda^{\frac{1}{\nu}}$ in Eq. 1 (Guikema and Goffelt, 2008). The new formulation of (1) is given as,

$$P(Y = y; \mu, \nu) = \frac{1}{S(\mu, \nu)} \left(\frac{\mu^{y}}{y!}\right)^{\nu}, \ y = 0, 1, 2, ..., \infty$$
(3)

where,

$$S(\mu,\nu) = \sum_{n=0}^{\infty} \left(\frac{\mu^n}{n!}\right)^{\nu}$$
(4)

The mean and variance of the distribution from Eq. 3 are derived as $E(Y) \approx \mu + \frac{1}{2}\nu - \frac{1}{2}$ and $Var(Y) \approx \frac{\mu}{\nu}$, it becomes accurate for $\mu > 10$ and $\nu \leq 1$ (Shmueli et al., 2005). Now, the new parameterization allows μ and ν as centering and shape parameters, respectively. The COMPRM consists of two types of models: the mean model and the dispersion model.

The COMP regression model is a dual-link GLM, as mean and variance depend on covariates. Y is the count variable (response variable), x_i and z_i are the covariates used in the mean link function and variance link function with p and q terms, respectively (Francis et al., 2012).

$$ln(\mu_i) = \beta_0 + \sum_{j=1}^p \beta_j x_{ij} = x_i^t \beta$$
(5)

$$ln(v_i) = \delta_0 + \sum_{k=1}^q \delta_k z_{ik} = z_i^t \delta$$
(6)

The mean and variance models in Eqs. 5 and 6 are used to estimate the coefficients of the COMPRM. For simplicity, we will assume a single value of v and use the mean model for estimation purposes. Let $\eta_i = log(\mu_i) = x'_i\beta$ is the linear predictor with a log link, where β is the vector of regression coefficients, including the intercept. Based on the new formulation, the likelihood function of Eq. 3 (Francis et al., 2012). The log-likelihood function can be written as

$$l(y_{i}; \beta, \nu) = \nu \sum_{i=1}^{n} y_{i} \eta_{i} - \sum_{i=1}^{n} \nu \log(y_{i}!) - \sum_{i=1}^{n} \log[S(\eta_{i}, \nu)]$$
(7)

For the estimation of parameters vector β and dispersion parameter v, we solve the log-likelihood function defined in Eq. 7. For this purpose, by differentiating Eq. 7 w.r.t β and ν , it becomes (Francis et al., 2012).

$$\frac{\partial l}{\partial \beta_j} = \sum_{i=1}^n (y_i \nu - \frac{\partial}{\partial \eta_i} \log[S(\eta_i, \nu)]) x_{ij}$$
(8)

$$\frac{\partial l}{\partial \nu} = \sum_{i=1}^{n} (-\log(y_i!) - \frac{\partial}{\partial \nu} \log[S(\eta_i, \nu)])$$
(9)

The solution to Eqs. 8 and 9 is obtained using the iterative reweighted least squares (IRLS) method (Sellers and Shmueli, 2010). To estimate the parameter β , it is necessary to fix v, and the same procedure applies to estimate the second parameter. For more details, refer to Shmueli et al. (2005). One disadvantage of using the MLE is that the variance becomes inflated when there is severe collinearity among the explanatory variables. Under these conditions, it becomes very difficult to determine whether the regression coefficients are significant. Fixing v, the maximum likelihood (ML) of β is,

$$\hat{\beta}_{MLE} = (S)^{-1} X^t \widehat{W} q, \tag{10}$$

where, $S = X^t \widehat{W}X$, $q = log(\widehat{\mu}) + \frac{(y-\widehat{\mu})}{Var(\widehat{\mu})}$ is a vector of the adjusted response variable, and \widehat{W} is a matrix of weights, i.e. $\widehat{W} = diag(V_i)$, where $V_i = \frac{\tau_i}{\nu} + \frac{v_i^2 - 1}{24v_i^3}\tau_i^{-1} + \frac{v_i^2 - 1}{12v_i^4}\tau_i^{-2} + \frac{v_i^2 - 1}{6v_i^5}\tau_i^{-3}$ with $\tau_i = \frac{\widehat{\mu}_i}{\nu}$. \widehat{V} and q both are evaluated by using the Fisher scoring procedure. The matrix MSE (MMSE) and scalar MSE of Eq. 10 are respectively given as,

$$MSE(\hat{\beta}_{MLE}) = E(\hat{\beta}_{MLE} - \beta)^{\iota}(\hat{\beta}_{MLE} - \beta)$$
$$MSE(\hat{\beta}_{MLE}) = \hat{v}tr(S) = \hat{v}\sum_{j=1}^{r} \frac{1}{\lambda_{i}'}$$
(11)

where, λ_j is the jth eigenvalue of the *S* matrix, $\hat{\nu}$ is estimated dispersion parameter.

a.,

2.2. The Stein estimator for COMP regression model

Stein (1960) proposed an estimator as a remedy for correlated regressors in the LRM. For the COMPRM, we proposed a Stein estimator to overcome the effect of correlated regressors. The proposed COMPSE is defined as:

$$\hat{\beta}_s = c\hat{\beta}_{MLE},\tag{12}$$

where, c (0 < c < 1) is the Stein parameter. When c=1, $\hat{\beta}_{COMPSE} = \hat{\beta}_{MLE}$. The estimated bias and covariance of Eq. 12 can be computed as,

$$Bias(\hat{\beta}_{s}) = E(\hat{\beta}_{s}) - \beta$$

$$Bias(\hat{\beta}_{s}) = c\beta - \beta$$

$$Bias = Bias(\hat{\beta}_{s}) = (c - I_{r})\beta,$$
(13)

where, I_r is the identity matrix of order $r \times r$. The variance of the COMPSE is calculated as,

$$Cov(\hat{\beta}_{s}) = c^{2}Cov(\hat{\beta}_{MLE})$$

$$MSE(\hat{\beta}_{s}) = Cov(\hat{\beta}_{s}) + Bias(\hat{\beta}_{s})^{2}$$

$$MSE(\hat{\beta}_{s}) = \hat{v}\sum_{j=1}^{r}\frac{c^{2}}{\lambda_{j}} + (c-1)^{2}\sum_{j=1}^{r}\alpha_{j}^{2},$$
(14)

where, α_j^2 is the jth element of $Q^t \hat{\beta}_{MLE}$ and Q is the eigenvector of the matrix $Q(\Lambda)Q^t$, where $\Lambda = diag(\lambda_j)$ and *c* is a biasing parameter of the COMPSE and λ_j are eigenvalues. The MSE of the COMPSE depends on the value of *c*. An appropriate value of the *c* yields the minimum MSE of the COMPSE. Therefore, we suggest some new estimating methods to estimate the value of *c* for the COMPSE in the next subsection.

2.3. Proposed biasing parameters

For the selection of the biasing parameter, an optimum value of the biasing parameter can be obtained by taking a derivative of Eq. 14 and equating it to zero,

$$\frac{\frac{\partial (MSE(\hat{\beta}_s))}{\partial c}}{\sum_{j=1}^{r} 2c(\hat{\nu} + \lambda_j \alpha_j^2)} = 2\sum_{j=1}^{r} \alpha_j^2 \lambda_j.$$

On simplification, we obtain the value of *c* as,

$$c = \frac{\sum_{j=1}^{r} \alpha_j^2 \lambda_j}{\sum_{j=1}^{r} \nu + \alpha_j^2 \lambda_j}.$$
(15)

Based on the work of Hoerl and Kennard (1970) and Kibria (2003), Eq. 15 generally can be written as

$$c_j = \frac{\alpha_j^2 \lambda_j}{\nu + \alpha_j^2 \lambda_j}$$

Furthermore, using the above expression, we proposed the following biasing parameters for the COMPSE,

$$c_1 = \max(c_j),\tag{16}$$

$$c_2 = \frac{\prod_{j=1}^r c_j^{(1/r)}}{\max(c_j)},\tag{17}$$

$$c_3 = \begin{pmatrix} 1 \\ - \end{pmatrix} \sum_{i=1}^r c_i, \tag{18}$$

$$c_4 = median(c_j), \tag{19}$$

$$c_5 = \prod_{j=1}^r c_j^{(1/r)}, \tag{20}$$

$$c_6 = \frac{\sum_{j=1}^{L_{j=1}} a_j}{\sum_{j=1}^{r} a_j^2 + \nu \sum_{j=1}^{r} \frac{1}{\lambda_j}}.$$
 (21)

2.4. The theoretical comparison of the proposed estimator

The superiority of the COMPSE is compared with the MLE using the following theorem.

Lemma 2.1: Let M be a positive definite (p.d.) matrix, a be a vector of nonzero constants and c be a positive constant. Then $cM - \alpha \alpha^t > 0$ if and only if $\alpha^t M \alpha < c$ (Farebrother, 1976).

Theorem 2.1: Under COMPSE, consider c > 0, $b_{COMPSE} = Bias(\hat{\beta}_{COMPSE})$ is the bias of COMPSE then $MSE(\hat{\beta}_{MLE}) - MSE(\hat{\beta}_{COMPSE}) > 0$ if $b_{COMPSE}[\hat{v}(S)^{-1} - \hat{v}c^2((S)^{-1})] b_{COMPSE}^t < 1.$

Proof: The difference in MSE from Eqs. 11 and 14 can be,

$$\Delta_1 = MMSE(\hat{\beta}_{MLE}) - MMSE(\hat{\beta}_{COMPSE})$$

= $\hat{v}[(S)^{-1} - c^2((S)^{-1})] - b_{COMPSE}b_{COMPSE}^t.$ (22)

From Eq. 22, we can write it as,

 $= \hat{v}(S)^{-1}[1-c^2] - b_{COMPSE}b_{COMPSE}^t$

The difference between the scalar MSE functions of MLE and COMPSE is as,

$$\begin{split} & MSE(\hat{\beta}_{MLE}) - MSE(\hat{\beta}_{COMPSE}) \\ &= \sum_{j=1}^{r} \left(\frac{\hat{v}}{\lambda_j} - \frac{\hat{v}c^2}{\lambda_j} + (c-1)^2 \alpha_j^2 \right) \\ &= \sum_{j=1}^{r} \left(\hat{v} \frac{(1-c^2)}{\lambda_j} + (c-1)^2 \alpha_j^2 \right) \end{split}$$

On simplifying the results, we get

$$MSE(\hat{\beta}_{MLE}) - MSE(\hat{\beta}_{COMPSE}) = \hat{v} \sum_{j=1}^{r} \left(\frac{(1-c^2) + \lambda_j(c-1)^2 \alpha_j^2}{\lambda_j} \right).$$

The expression $\hat{v}[(S)^{-1}c^2]$ is p.d if $[1-c^2] > 0$. Thus if 0 < c < 1, then the theorem is completed by Lemma 2.1 and it is enough to prove that the COMPSE is superior to the MLE in the form of scalar MSE for the COMPRM.

3. Monte Carlo simulation study

This section contains a numerical evaluation of the proposed estimator and a comparison with MLE using a Monte Carlo simulation. For this purpose, various factors are taken with different values. These factors include sample size, dispersion, correlated regressors, and the number of explanatory variables. The assumed values of these factors are given in Table 1.

 Table 1: Assumed values of different factors for simulation

study							
Factors	Notation	Values					
Number of explanatory variables	р	3,6,9,12					
Number of replicates	R	1000					
Dispersion parameter	v	0.85,1,1.25					
Sample size	n	50,100,150,200					
Degree of correlation	ρ^2	0.8,0.9,0.95,0.99					

The response variable of the COMPRM is generated from a *CMP* (μ_i , ν) distribution, where:

$$\mu_{i} = exp(\beta_{0} + \beta_{1}x_{i1} + \dots + \beta_{p}x_{ip}), \quad i = 1, \dots, n.$$
(23)

The correlated explanatory variables are generated as follows (Kibria, 2003).

$$x_{ij} = (1 - \rho^2)^{1/2} z_{ij} + \rho z_{i(j+1)}, i = 1, \dots, n; j = 1, \dots, p.$$
 (24)

where, z_{ij} are the independent standard normal pseudo-random numbers. The regression parameters are selected in such a way that $\sum_{j=1}^{p} \beta_j^2 = 1$, which is a commonly used restriction in the field (Amin et al., 2023b). For the different combinations of n, p, ρ, v , the data is repeatedly generated 1000 times. The MSE criteria is used to gauge the performance of the estimators, which is defined by,

$$MSE(\hat{\beta}) = \frac{\sum_{i=1}^{R} (\hat{\beta}_i - \beta)^{t} (\hat{\beta}_i - \beta)}{R},$$
(25)

where, $(\hat{\beta}_i - \beta)$ is the difference between the true parameter and estimated vectors of the proposed and other considered estimators at *i*th replication, and *R* represents the number of replications.

3.1. Results and discussions

The simulation study is performed under the various factors listed in Table 1. The estimated MSEs of the considered estimators are given in Tables 2-13. The summary of simulation results is as follows,

- Table 2 presents the estimated mean square error (EMSE) for p=3 and v=0.85 for the overdispersion case. It is observed that COMPSE with c_5 at sample size n=50,100,150, and 200 has minimum EMSE for all levels of multicollinearity as compared to the MLE and COMPSE with all other proposed Stien parameter estimators.
- On comparing the results of the proposed estimator concerning sample size, it is observed that an increase in sample size causes a decrease in the values of EMSEs. From Table 2, it is observed that for a fixed level of multicollinearity 0.80, *p*=3, and *v*=0.85, the EMSEs are 0.8777, 0.8440, 0.8835, and 0.8484, respectively. Hence, the gradual decrease in values of EMSEs shows the efficiency of the proposed estimator to combat multicollinearity by increasing the sample size.
- From Table 3, for all levels of multicollinearity, when p=3, v=1, and n=50, the values of EMSEs of c_5 are 0.9797, 1.6971, 1.8197 and 5.8784. So, the performance as a function of multicollinearity for the fixed *n*, *p*, and *v* shows an increasing trend as

the level of multicollinearity increases for the EMSE of the COMPSE. The same pattern is observed in Tables 2-13.

• Tables 2, 5, 8, and 11 present the EMSE for *p*=3, 6, 9, and 12, respectively, showing that as the number of explanatory variables increases, the EMSEs of the estimators also increase. For *p*=*3*, Tables 2, 3, and 4 represent the estimated MSE for overdispersion, equidispersion, and underdispersion, respectively. The results clearly show that the EMSE is the least affected by overdispersion as compared to the equal and under-dispersion cases.

4. Application: Plastic plywood data

In this section, the performance of the proposed estimator is evaluated with the help of a real-life dataset that is related to the plastic plywood dataset. This application was considered by many researchers with different variables (Azaman et al., 2013; Demirkir et al., 2013; Fang et al., 2014). We consider this application to evaluate the performance of our proposed method and compare it with the MLE. This application consists of n=100observations, where the response variable y represents the number of defects that may increase or decrease per laminated plastic plywood area. The four explanatory variables include volumetric shrinkage (x_1) , assembly time (x_2) , wood density (x_3) and drying temperature (x_4) .

The estimated dispersion parameter is found to be $\hat{v} = 0.9614$, which indicates that there is overdispersion in the data set. In the regression model, commonly used methods are variance inflation factor (VIF) and condition index (CI) to test multicollinearity among the explanatory the variables. The $CI = \sqrt{\lambda_{max}/\lambda_{min}} = 8634.73$ of this data set shows severe multicollinearity among the explanatory variables. Hence, we use the COMPSE to overcome the effect of correlated explanatory variables in the COMPRM. The MSEs of the MLE and COMPSE with different shrinkage parameters are computed using Eqs. 11 and 14, respectively. The estimated regression coefficients and MSEs of different shrinkage parameters of the MLE, COMPSE are mentioned in Table 14. On comparing the performance of the COMPRM estimators, it is observed that our newly proposed estimator (COMPSE) with all five Stein parameters outperforms as compared to the MLE. Furthermore, when there are highly correlated regressors, MLE is the estimator that is most negatively affected.

5. Conclusion

In this study, we introduced a new estimator, the COMPSE, for the COMPRM to reduce the impact of correlated regressors. We evaluated the proposed estimator using a Monte Carlo simulation study, with the EMSE as the performance criterion, where a lower EMSE indicates better performance.

Table 2: EMSEs for v = 0.85 and p=3

n	o^2				COMPSE			
	P	MLE	<i>C</i> ₁	<i>C</i> ₂	<i>C</i> ₃	C_4	C ₅	C ₆
50	0.8	1.8731	1.8540	0.8804	0.8810	1.0033	0.8777	1.0032
	0.9	3 7777	3 74.05	1 3522	1 6757	1 9509	1 3453	1 9268
	0.7	6 2026	(222)	2 1001	2 0 2 2 2	2 5 1 5 5	2 1021	2.0700
	0.95	6.3936	0.3320	2.1981	2.9232	3.5155	2.1831	2.9709
	0.99	36.5167	36.248	9.7654	16.282	20.312	9.6973	14.9107
100	0.8	1.6016	1.5950	0.8449	0.8377	0.9673	0.8440	0.9471
	0.9	3,2445	3,2312	1,2556	1.5366	1.8255	1.2531	1.7311
	0.95	5 9275	5 9035	1 9772	2 7852	3 4 5 3 0	1 9718	2 9880
	0.75	20.07273	20.7512	0.1200	15 211	10 717	0.1046	2.7000
450	0.99	30.8720	30.7512	9.1390	15.511	19.717	9.1040	14.0008
150	0.8	1.7464	1.7419	0.8842	0.9127	1.0502	0.8835	1.0923
	0.9	2.8779	2.8707	1.2421	1.4511	1.7099	1.2405	1.6625
	0.95	5.6424	5.6276	1.9006	2.7152	3.4022	1.8974	3.0410
	0 99	24 2021	24 1431	6 2 1 3 0	11 498	15 362	6 1995	10 9629
200	0.55	1 6 2 2 0	1 6 2 0 0	0.0400	0.0405	0.0072	0.0100	1 0 2 0 2
200	0.8	1.0339	1.0308	0.8488	0.8685	0.9875	0.0404	1.0202
	0.9	3.1381	3.1319	1.2212	1.5147	1.8416	1.2200	1.7888
	0.95	5.7624	5.7516	2.0636	2.8449	3.4706	2.0610	3.0242
	0.99	20.2210	18.2341	5.1223	10.2120	14.7563	5.0100	10.1180
			Bol	d indicated the sm	aller EMSE			
			Table	2. FMSEs for v	-1 and $n=3$			
-			Table	J. LM3L3 101 /	-1 and $p-3$			
n	0 ²				COMPSE			
11	Ρ	MLE	<i>C</i> ₁	C_2	C3	C_4	C5	C ₆
50	0.8	2.5216	2,4943	0.9838	1.0589	1.1279	0.9797	1.2586
55	0.0	1.2002	1.7600	1 7066	2 0852	2 4005	1 6071	2 3400
	0.7	4.5004	4.4007	1.7000	2.0037	2.4093	1.07/1	2.3400
	0.95	6.1630	6.1047	1.8304	2.69/3	3.3640	1.8197	2./369
	0.99	32.3845	32.1564	5.9207	13.202	17.2830	5.8784	12.9325
100	0.8	1.5628	1.5558	0.8833	0.8280	0.9490	0.8823	0.9180
	0.9	3.6075	3.5937	1.4076	1.7506	2.0526	1.4047	2.0296
	0.05	6 3 3 6 1	6 3088	1 9269	2 8300	3 5250	1 9215	2 9814
	0.95	0.0004	21 4010	0.0775	4.0377	20.0600	0 6484	14 (645
	0.99	31.6043	31.4819	8.6//5	15.6335	20.8690	8.0450	14.0045
150	0.8	1.5385	1.5344	0.8700	0.8412	0.9892	0.8695	0.9504
	0.9	3.0156	3.0077	1.0583	1.3934	1.7623	1.0572	1.6466
	0.95	5.9811	5,9659	2.2116	3.0050	3.7501	2.2077	3.1833
	0.99	30 9721	30 8964	8 5471	15 0428	19 7190	8 5288	15 1740
200	0.77	17666	17(22	0.07(0	0.0050	1 1 5 2 0	0.0260	1 1 2 4 5
200	0.8	1./000	1./032	0.9769	0.9950	1.1539	0.9762	1.1245
	0.9	3.0860	3.0800	1.1884	1.5256	1.9210	1.1873	1.7502
	0.95	5.2988	5.2891	2.0396	2.7508	3.3882	2.0371	2.9301
	0.99	26.1379	26.0902	7.3227	12.9054	17.1422	7.3106	12.8037
			Bol	d indicated the sm	aller EMSE			
			201	a marcatea are om				
			Table 4.	EMCEs form	- 1 25 and n-2			
			Table 4:	EMSESIOI V =	= 1.25 and p=5			
	o ²				COMPSE			
п	ρ —	MLE	C1	C_2	C3	C _A	Cs	C6
50	0.8	3 6527	3 5115	1 1557	1 3714	1 5082	1 1 2 8 2	1 3/13/1
50	0.0	0.0527	3.3113	1.1337	1.5714	1.3002	1.1303	1.3434
	0.9	8.3539	8.0320	1./9/1	2.7803	2.9743	1.7514	2.4/08
	0.95	15.0446	14.4979	3.6317	5.6743	6.4204	3.5207	4.3157
	0.99	82.8496	81.0760	18.7003	32.9074	38.3932	18.2613	22.5578
100	0.8	3.9743	3.9003	1.2142	1.5167	1.6707	1.2051	1.6109
	0.9	6 6 2 5 9	6 5054	1 4900	2 4166	2 7908	1 4765	2 2696
	0.05	12 4725	12 2204	2 7021	E 1426	6 1001	2 7562	2.2070
	0.95	13.4733	15.2594	2.7931	5.1450	0.1901	2.7505	3.9040
	0.99	69.8082	68./806	10.9614	28.0143	36.///6	10.7996	19.0875
150	0.8	3.7132	3.6685	1.1713	1.4597	1.6050	1.1657	1.5676
	0.9	5.7822	5.7136	1.4829	2.0971	2.3049	1.4741	1.9301
	0.95	11.4546	11.3204	2.2450	4.2160	5.0250	2.2270	3.3182
	0.99	65 2814	64 6202	11.0595	25 9822	33 6440	10 9467	19.6371
200	0.99	2 52/1	2 5025	1 2602	1 1 502	1 5577	1 9555	1 50071
200	0.0	0.0041	2.2022	1.2003	1.4302	1.3374	1.4333	1.3447
	0.9	0.0415	5.9888	1./040	2.359/	2.64/0	1.0952	1.995/
	0.95	11.8783	11.7739	2.8339	4.8364	5.9326	2.8151	4.0940
	0.99	61.9594	61.4578	15.6510	27.4905	34.2896	<u>15.528</u> 7	18.7061
			Bol	d indicated the sm	aller EMSE	· · · · ·		
			Table 5	EMSEs for y -	= 0.85 and $n=6$			
			Table J.	- / 101 613 101 /	COMPCE			
n	ρ^2 —				COMPSE			
	٣	MLE	<i>c</i> ₁	C2	c_3	<i>C</i> ₄	<i>C</i> ₅	<i>C</i> ₆
50	0.8	5.5244	5.4716	1.3559	1.8922	2.0588	1.3504	2.3479
	0.9	10.0862	9 9881	1 7698	3 0566	3 3763	1 7598	3 5456
	0.0	20.0000	21 4022	1.0075	7 2244	0 2026	2 0010	7 0502
	0.95	21./299	41.4943	4.02/5	/.2244	0.3020	3.9910	1.9582
	0.99	97.0780	96.3202	12.2767	28.0876	28.1059	12.2013	28.9626
100	0.8	4.4131	4.3941	1.1299	1.5226	1.7268	1.1280	2.049
	0.9	8.0001	7.9648	1.5735	2.66216	2.9933	1.5696	3.2710
	0.95	13.8590	13,7984	2.6634	4,4330	4,4197	2.6549	5,4104
	0.90	70 3545	70.0592	11 1222	23 160	26 6672	11 0010	25 5155
150	0.77	/0.3343	10.0383	11.1222	40.109	40.00/3	11.0010	40.5155
150	0.8	4.0898	4.0784	1.1505	1.4857	1.6306	1.1492	1.9053
	0.9	6.7151	6.6967	1.3993	2.2573	2.5946	1.3974	2.9771
	0.95	11.3812	11.3530	2.3845	4.1255	4.8588	2.3804	5.0517
	0.99	64.0067	63.8508	12.0997	22,4253	23,2276	12.0724	26.1653
200	0.8	3 6062	3 5901	1 0294	1 3140	1 4/93	1 0297	1 7550
200	0.0	6.0126	6 0001	1.0474	1.3147	2.7723	1.0407	1./ 330
	0.9	6.9126	0.8991	1.6564	2.5376	2.9479	1.6546	3.3209
	0.05	11 010	11 5596	2 1800	3 9879	4.2929	2 1 7 7 2	4 8047
	0.95	11.3010	11.5570	2.1000	5.707 7		4.1//4	1.0017
	0.95	61.2940	61.1754	8.4401	20.4894	24.8705	8.4255	25.8117
	0.95	61.2940	61.1754 Bol	8.4401 d indicated the sm	20.4894 aller EMSE	24.8705	8.4255	25.8117

Table 6: EMSEs for v = 1 and p=6

n	o^2				COMPSE			
	Ρ	MLE	<i>C</i> ₁	<i>C</i> ₂	<i>C</i> ₃	<i>C</i> ₄	C ₅	<i>C</i> ₆
50	0.8	9.7380	9.5465	1.2930	2.2997	2.2568	1.2812	2.6322
	0.9	16.7992	16.4948	2.4856	4.6955	4.7940	2.4543	4.9610
	0.95	29.3329	28.7969	3.3275	7.3523	7.0641	3.2781	7,0416
	0.99	158 2569	156 1642	16 2835	40.8691	34,8033	16 0679	36 7931
100	0.99	5 1600	5 / 1042	1 0.2033	1 5/10	1 5202	10759	1 0221
100	0.0	100507	J.4173	1.0/04	1.5410	2 4 6 9 7	1 0000	1.0331
	0.9	10.8507	10.7598	1.81/6	3.1/37	5.4687	1.8089	3.5306
	0.95	19.6763	19.5097	3.1715	5.6516	5.3441	3.1510	5.9439
	0.99	102.6834	101.993	14.5491	31.1315	29.3552	14.4592	30.7586
150	0.8	4.8208	4.7946	1.1193	1.5207	1.6000	1.1171	1.8253
	0.9	8.2393	8.1952	1.3440	2.2222	2.1182	1.3409	2.5607
	0.95	18.2975	18.1992	2.7970	5.4004	5.3754	2.7861	5.9125
	0.99	88.0189	87,5731	12,8577	25,7513	24.5624	12,7971	26.6877
200	0.8	4 5940	4 5759	1 0258	1 3803	1 3820	1 0247	1 6945
200	0.0	10 0725	10.0227	1.0250	2 0711	2 2 4 2 9	1.0247	2 6242
	0.9	10.0723	16.0327	1.0709	3.0711	3.2420	1.0003	5.0242
	0.95	16.2784	16.2148	2.3754	4.8462	4.9285	2.3688	5./353
	0.99	/3.5241	/3.2503	9.5098	21.1291	21.1951	9.4776	21.0472
			В	old indicated the sn	naller EMSE			
					4.05 1 6			
			Table '	7: EMSEs for ν :	= 1.25 and <i>p</i> =6			
	- 2				COMPSE			
n	ρ^2	MLE	C1	C2	C2	C4	Cr	Cc
50	0.8	12 4644	11 9755	1 6703	2 8483	2 7768	1 6299	3 0068
50	0.0	2.7077	22 2601	2 6024	5 5100	2.7700 4.7107	2 2260	5.0000
	0.9	42 0464	42 25.2001	4.0054	0.6500	7.7107	2.3300	0.0796
	0.95	43.8464	42.3519	4.0853	9.0509	7.2007	3.9/30	0.0720
400	0.99	242.5266	237.045	23./3/2	57.3941	50.6290	23.1779	45.0071
100	0.8	8.5819	8.4198	1.2109	2.0600	1.9042	1.2029	2.1939
	0.9	16.8357	16.5257	2.1273	4.1330	3.8733	2.1009	4.0861
	0.95	29.1483	28.6094	3.0947	6.6175	5.5064	3.0514	5.7289
	0.99	143.819	141.6595	13.1633	34.3678	27.7705	12.9960	28.6092
150	0.8	7.9381	7.8411	1.2152	1.9477	1.8511	1.2099	2.1776
	0.9	14.2010	14.0362	1.7782	3.5553	3.5147	1.7672	3.7716
	0.95	27.8953	27.5761	3.3276	6.8072	5.5076	3.2995	6.6319
	0.99	125 6663	124 3192	10 7117	29 5072	21.864.8	10 6022	23 5085
200	0.55	8 1052	8 03/1	1 / 220	2 1 1 2 1	21.0040	1 4.272	23.3003
200	0.0	1/ 0/00	1/ 720/	1.4367	2.1101	2.0103	1.74/4 2 1024	2.3341
	0.9	14.0090	14./390	2.1142	3.82//	3.3358	2.1021	3.7285
	0.95	21.4289	21.2401	2.0310	4./601	4.3053	2.0201	4.3892
	0.99	129.477	128.5728	10.4659	29.9874	23.5663	10.3983	30.4567
			В	old indicated the sn	naller EMSE			
				0 01/0	0.0F			
			<u> </u>	B: EMSEs for <i>v</i> :	<u>= 0.85 and p</u> =9			
	2				COMPSE			
n	ρ^2	MLE	C1	Ca	C2	C.	Cr	C,
50	0.0	12 17/2	12 0/12	1 6200	2 0 2 9 7	2 1066	1 6104	4 04.94
50			14.0414	1.0200	3.030/	5.1900	1.0104	4.0474
	0.8	20 1100	10,0000	2 1 20 5		5 111111		n I /h/
	0.8	20.1100	19.8980	2.4295	4.8854	11 5000	2.4120	12 2602
	0.8 0.9 0.95	20.1100 44.9510	19.8980 44.4881	2.4295 4.7080	11.5664	11.5920	2.4120 4.6714	13.3608
	0.8 0.9 0.95 0.99	20.1100 44.9510 189.7279	19.8980 44.4881 188.2678	2.4295 4.7080 15.8642	4.8852 11.5664 45.5422	11.5920 43.5135	2.4120 4.6714 15.7598	13.3608 46.8489
100	0.8 0.9 0.95 0.99 0.8	20.1100 44.9510 189.7279 7.9619	19.8980 44.4881 188.2678 7.9266	2.4295 4.7080 15.8642 1.3268	4.8852 11.5664 45.5422 2.1726	11.5920 43.5135 2.1689	2.4120 4.6714 15.7598 1.3240	13.3608 46.8489 2.9569
100	0.8 0.9 0.95 0.99 0.8 0.9	20.1100 44.9510 189.7279 7.9619 15.27	19.8980 44.4881 188.2678 7.9266 15.1989	2.4295 4.7080 15.8642 1.3268 1.9019	4.8852 11.5664 45.5422 2.1726 3.9662	11.5920 43.5135 2.1689 4.0940	2.4120 4.6714 15.7598 1.3240 1.8964	13.3608 46.8489 2.9569 5.3999
100	0.8 0.9 0.95 0.99 0.8 0.9 0.95	20.1100 44.9510 189.7279 7.9619 15.27 27.2705	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739	11.5920 43.5135 2.1689 4.0940 6.1911	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166	13.3608 46.8489 2.9569 5.3999 8.7935
100	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322	4.8832 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562	$\begin{array}{c} 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779	13.3608 46.8489 2.9569 5.3999 8.7935 42.0009
100 150	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713	$\begin{array}{c} 3.6000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993	13.3608 46.8489 2.9569 5.3999 8.7935 42.0009 3.3992
100 150	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912	11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058	$\begin{array}{c} 1.132\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\end{array}$
100 150	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30 5325	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451	11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483 8.6224	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4 4303	$\begin{array}{c} 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11\ 1534\end{array}$
100 150	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.95 0.99	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304 \end{array}$	$19.8980 \\ 44.4881 \\ 188.2678 \\ 7.9266 \\ 15.1989 \\ 27.1466 \\ 131.0075 \\ 8.8954 \\ 14.1451 \\ 30.5325 \\ 156.641 \\ 156.641 \\ 10000000000000000000000000000000000$	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0263	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419	11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483 8.6224 43.4421	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511	13.3608 46.8489 2.9569 5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56 3899
100 150	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.95 0.99	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6927\end{array}$	$19.8980 \\ 44.4881 \\ 188.2678 \\ 7.9266 \\ 15.1989 \\ 27.1466 \\ 131.0075 \\ 8.8954 \\ 14.1451 \\ 30.5325 \\ 156.641 \\ 7.664 \\ 15.644 \\ 10.5325 \\ 156.641 \\ 10.5325$	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.2620	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2029	$\begin{array}{c} 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.2042\end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.05111 1.2616	13.3608 46.8489 2.9569 5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764
100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9$	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4262\end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.2052	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2025	11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043 5.0522	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426	$\begin{array}{c} 8.1762\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 4.1972\end{array}$
100 150 200	0.8 0.9 0.95 0.99 0.8 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 20.4127\end{array}$	$\begin{array}{c} 19.8980\\ 44.4881\\ 188.2678\\ 7.9266\\ 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\\ 20.2021\end{array}$	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 2.0045	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.0001	$\begin{array}{c} 13.5020\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 6.1427\end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 2.1426	$\begin{array}{c} 1.3.3608\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5162\end{array}$
100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\$	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 28.4487\\ 28.4487\\ 28.645\end{array}$	$19.8980 \\ 44.4881 \\ 188.2678 \\ 7.9266 \\ 15.1989 \\ 27.1466 \\ 131.0075 \\ 8.8954 \\ 14.1451 \\ 30.5325 \\ 156.641 \\ 7.6684 \\ 15.3952 \\ 28.3901 \\ 28.39$	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984	$\begin{array}{c} 13.5020\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 8.1217\end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902	$\begin{array}{c} 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 10.5169\end{array}$
100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\$	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 143.018\\ \end{array}$	$\begin{array}{c} 19.8980\\ 44.4881\\ 188.2678\\ 7.9266\\ 15.1989\\ 27.1466\\ 131.0075\\ 8.8954\\ 14.1451\\ 30.5325\\ 156.641\\ 7.6684\\ 15.3952\\ 28.3901\\ 142.7522\end{array}$	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749	$\begin{array}{c} 11.5920\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	$\begin{array}{c} 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804 \end{array}$
100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\end{array}$	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 143.018\\ \end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 maller EMSE	$\begin{array}{c} 3.6000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\end{array}$	$\begin{array}{c} 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804 \end{array}$
100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\end{array}$	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 143.018\\ \end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 maller EMSE	$\begin{array}{c} 13.5020\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061 \end{array}$	$\begin{array}{c} 1.3.3608\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804 \end{array}$
100 150 200	0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.95 0.99 0.8 0.95 0.99 0.8 0.9 0.95 0.99 0.8	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 143.018\\ \end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 maller EMSE v = 1 and $p=9$	11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043 5.0588 8.1217 41.3574	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \end{array}$	$\begin{array}{c} 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \end{array}$
100 150 200	0.8 0.9 0.95 0.99 0.8 0.99 0.95 0.99 0.8 0.95 0.99 0.8 0.99 0.8 0.95 0.99 0.8 0.99 0.95 0.99 0.99 0.95 0.99 0.99 0.95 0.99 0.99 0.95 0.99 0.90 0	$\begin{array}{c} 12.1742\\ 20.1100\\ 44.9510\\ 189.7279\\ 7.9619\\ 15.27\\ 27.2705\\ 131.5003\\ 8.9205\\ 14.1834\\ 30.6178\\ 157.0304\\ 7.6837\\ 15.4263\\ 28.4487\\ 143.018\\ \end{array}$	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 naller EMSE $\gamma = 1$ and $p=9$ COMPSE	$\begin{array}{c} 13.0303\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \end{array}$	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	$\begin{array}{c} 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \end{array}$
100 150 200 n	ho 0.8 0.9 0.95 0.99 0.8 0.97 0.99 0.8 0.97 0.99 0.8 0.99 0.8 0.99 0.95 0.99 0.8 0.99 0.8 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn	4.8852 11.5664 45.5422 2.1726 3.9662 6.6739 35.2562 2.4713 3.8912 8.6451 42.8419 2.2028 4.5035 7.9984 39.3749 haller EMSE v = 1 and $p=9COMPSE$	11.5920 11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043 5.0588 8.1217 41.3574	2.4120 4.6714 15.7598 1.3240 1.8964 3.1166 15.2779 1.3993 2.1058 4.4303 19.0511 1.3616 2.1426 3.8902 16.3061	13.3608 46.8489 2.9569 5.3999 8.7935 42.0009 3.3992 5.2536 11.1534 56.3899 3.1764 6.1252 10.5169 51.0804
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline\end{array}$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table	$\begin{array}{r} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ told indicated the sn \\ e 9: EMSEs for 1 \\ \hline c_2 \\ 1.6404 \end{array}$	$\begin{array}{r} 4.8852 \\ 11.5664 \\ 45.5422 \\ 2.1726 \\ 3.9662 \\ 6.6739 \\ 35.2562 \\ 2.4713 \\ 3.8912 \\ 8.6451 \\ 42.8419 \\ 2.2028 \\ 4.5035 \\ 7.9984 \\ 39.3749 \\ \text{naller EMSE} \\ \mu = 1 \text{ and } p=9 \\ \hline \begin{array}{r} c \\ c \\ c \\ c \\ 3 \\ 5 \\ 9 \\ 2 \\ \hline \end{array}$	11.5920 43.5135 2.1689 4.0940 6.1911 36.1952 2.4747 3.9483 8.6224 43.4421 2.3043 5.0588 8.1217 41.3574	$\begin{array}{r} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 0.1762\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50	$\rho^{0.8}$ 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.95 0.99 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.9 0.8 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.8 0.9 0.8 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 20.5295	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table c ₁	$\begin{array}{c} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ told indicated the sn \\ \hline e 9: EMSEs for 1 \\ \hline c_2 \\ \hline c_2 \\ 1.6494 \\ 2.9047 \\ \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \nu = 1 \text{ and } p=9\\ \hline \begin{array}{c} \\ COMPSE\\ \hline \\ c_3\\ \hline \\ 3.5982\\ 6.4574 \end{array}$	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} 0.1762\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50	$\rho^{2} = \frac{0.8}{0.9}$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0342	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table	$\begin{array}{c} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ 0 d \text{ indicated the sn} \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \hline compse\\ \hline \hline c_3\\ 3.5982\\ 6.4574\\ 11.2022\end{array}$	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1769 \\ 13.3608 \\ 46.8489 \\ 2.9569 \\ 5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ $
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline \end{array}$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.684 15.3952 28.3901 142.7522 B Table 	$\begin{array}{r} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ \hline the side of th$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \begin{array}{r} \nu = 1 \text{ and } p=9\\ \hline \text{COMPSE}\\ \hline c_3\\ \hline 3.5982\\ 6.4574\\ 11.2609\\ \hline \end{array}$	$\begin{array}{c} 3.6000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{r} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} 13.3608\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ \hline \end{array}$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table 	$\begin{array}{r} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ 0 d indicated the sn \\ \hline e 9: EMSEs for 1 \\ \hline c_2 \\ 1.6494 \\ 2.8947 \\ 3.8033 \\ 26.6251 \\ \hline \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \hline comPSE\\ \hline \hline c_3\\ 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ \hline \end{array}$	$\begin{array}{c} 13.5920\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} & .1763 \\ 13.3608 \\ 46.8489 \\ 2.9569 \\ 5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ $
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.8\\ 0.9\\ 0.8\\ 0.8\\ 0.8\\ 0.9\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table <u>c₁</u> 17.8366 29.9479 56.0273 312.7813 11.7589	$\begin{array}{c} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ told indicated the snee of the second s$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \begin{array}{c} c\\ c\\ c\\ c\\ s\\ s\\$	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.8\\ 0.9\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032	$\begin{array}{c} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ \hline the size of the s$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 4.5035\\ 7.9984\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \ maller EMSE\\ \hline \ \nu = 1 \ and \ p=9\\ \hline \ \ \ \ \ \ \ \ \ \ \ \ \$	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1769 \\ 13.3608 \\ 46.8489 \\ 2.9569 \\ 5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ $
100 150 200 <u>n</u> 50 100	$ \begin{array}{c} 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.684 15.3952 28.3901 142.7522 B Table 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942	$\begin{array}{c} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ \hline \begin{array}{c} 0d indicated the sn\\ 2 \mbox{ 9: EMSEs for 1}\\ \hline \\ \hline \\ c_2\\ \hline 1.6494\\ 2.8947\\ 3.8033\\ 26.6251\\ 1.3819\\ 2.2728\\ 3.2184\\ \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ \hline \nu = 1 \text{ and } p=9\\ \hline \hline compse\\ \hline c_3\\ 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ \hline \end{array}$	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} & .1763 \\ 13.3608 \\ 46.8489 \\ 2.9569 \\ 5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \\ $
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.99\\ 0.99\\ 0.95\\ 0.99\\ 0.9$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018 MLE 18.2156 30.5285 57.0240 315.518 11.8646 20.4850 37.6053 186.9961	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C ₁ 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586	$\begin{array}{r} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ old indicated the sn\\ \hline e 9: EMSEs for 1\\ \hline \hline c_2\\ 1.6494\\ 2.8947\\ 3.8033\\ 26.6251\\ 1.3819\\ 2.2728\\ 3.2184\\ 14.221\\ \hline \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ 1.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ 1.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ 1.2028\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ \hline \end{array}$	$\begin{array}{c} 13.5020\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \\ \hline$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.8\\ 0.9\\ 0.9\\ 0.8\\ 0.8\\ 0.9\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8\\ 0.8$	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12 2252	$\begin{array}{c} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ \hline \ $	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \begin{array}{c} \\ \hline \\ $	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150	$ \begin{array}{c} 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.9 \\ 0.8 \\ 0.9 \\ 0.8 \\ 0.9 \\ $	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table <u>c_1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6252	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn 2 9: EMSEs for 1 c ₂ 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \ maller EMSE\\ \textbf{v} = 1 \ and \ p=9\\ \hline \hline \ \ comPSE\\ \hline \ \ c_3\\ \hline \ \ 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ \hline \ \ \ \ \ \ \ \ \ \ \ \ \$	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \\ \hline \\ \hline \\ \hline \\ \\ \hline \\ \\ \hline \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \hline \\ \hline \\ \hline \\ \\ \hline \\ \hline \\ \hline \\ \hline \\ \\ \hline \\ \hline \\ \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \\ \hline \hline \\ \hline \\ \hline \\ \hline \\ \hline \hline \\ \hline \\ \hline \\ \hline \hline \\ \hline \\ \hline \hline \\ \hline \\ \hline \\ \hline \hline \\ \hline \hline \\ \hline \\ \hline \hline \\ \hline \\ \hline \\ \hline \hline \hline \\ \hline \hline \\ \hline \hline \hline \\ \hline \hline \\ \hline \hline \hline \\ \hline \hline \hline \\ \hline \hline \hline \hline \hline \\ \hline \hline \hline \hline \hline \\ \hline \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1769 \\ 13.3608 \\ 46.8489 \\ 2.9569 \\ 5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150	$ \begin{array}{c} 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.99 \\ 0.8 \\ 0.9 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.90 \\ 0.95 \\ $	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.684 15.3952 28.3901 142.7522 B Table 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn 2 9: EMSEs for 1 c ₂ 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2917	$\begin{array}{r} 4.8852 \\ 11.5664 \\ 45.5422 \\ 2.1726 \\ 3.9662 \\ 6.6739 \\ 35.2562 \\ 2.4713 \\ 3.8912 \\ 8.6451 \\ 42.8419 \\ 2.2028 \\ 4.5035 \\ 7.9984 \\ 39.3749 \\ \hline \\ maller EMSE \\ \hline \\ \nu = 1 \ and \ p=9 \\ \hline \\ $	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \\ \hline$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.8\\ 0.9\\ 0.95\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\ 0.90\\$	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C ₁ 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662	$\begin{array}{c} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ \hline \\ old indicated the sn \\ \hline e 9: EMSEs for 1 \\ \hline \\ \hline \\ e 9: EMSEs for 1 \\ \hline \\ c_2 \\ 1.6494 \\ 2.8947 \\ 3.8033 \\ 26.6251 \\ 1.3819 \\ 2.2728 \\ 3.2184 \\ 14.221 \\ 1.6152 \\ 2.4081 \\ 4.2817 \\ \hline \\ 1.675 \\ \hline \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \hline v = 1 \text{ and } p=9\\ \hline compse\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_3\\ \hline c_686\\ 4.7265\\ 7.9611\\ \hline c_686\\ 4.7265\\ 7.9611\\ \hline c_686\\ 4.7265\\ 7.9611\\ \hline c_755\\ \hline c_755\\ \hline c_686\\ 4.7265\\ 7.9611\\ \hline c_755\\ \hline c_755\\ \hline c_686\\ 4.7265\\ 7.9611\\ \hline c_755\\ \hline c_755\\ \hline c_755\\ \hline c_75\\ \hline c_75\\ \hline c_755\\ \hline c_75\\ \hline c_75\\$	$\begin{array}{c} 1.5920\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & 1.33608 \\ 13.3608 \\ 46.8489 \\ 2.9569 \\ 5.3999 \\ 8.7935 \\ 42.0009 \\ 3.3992 \\ 5.2536 \\ 11.1534 \\ 56.3899 \\ 3.1764 \\ 6.1252 \\ 10.5169 \\ 51.0804 \\ \end{array}$
100 150 200 <u>n</u> 50 100 150	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\$	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table <u>C1</u> 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504	$\begin{array}{r} 2.4295 \\ 4.7080 \\ 15.8642 \\ 1.3268 \\ 1.9019 \\ 3.1270 \\ 15.3322 \\ 1.4012 \\ 2.1094 \\ 4.4406 \\ 19.0963 \\ 1.3629 \\ 2.1455 \\ 3.8966 \\ 16.3336 \\ 0 d indicated the sn \\ \hline e 9: EMSEs for 1 \\ \hline \hline c_2 \\ 1.6494 \\ 2.8947 \\ 3.8033 \\ 26.6251 \\ 1.3819 \\ 2.2728 \\ 3.2184 \\ 14.221 \\ 1.6152 \\ 2.4081 \\ 4.2817 \\ 16.1405 \\ \hline \end{array}$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \hline comPSE\\ \hline c_3\\ \hline c_3\\ \hline comPSE\\ \hline c_3\\ \hline c.35982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ \hline \end{array}$	$\begin{array}{c} 13.5020\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150 200	$\rho^{2} = \frac{\rho^{2}}{\rho^{2}}$	20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table c ₁ 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504 10.6662	$\begin{array}{c} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ \hline old indicated the sneet of t$	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 4.5035\\ 7.9984\\ 4.5035\\ 7.9984\\ 9.3749\\ \text{maller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \hline \begin{array}{c} \\ \hline \\ $	$\begin{array}{c} 3.5000\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9\\ 0.9$	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.684 15.3952 28.3901 142.7522 B Table 28.3901 142.7522 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504 10.6662 20.7545	$\begin{array}{c} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ old indicated the sn\\ 2 9: EMSEs for 1\\ \hline $	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \hline \\ \mbox{mailer EMSE}\\ mail$	$\begin{array}{c} 13.5020\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \hline \end{array}$
100 150 200 <u>n</u> 50 100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.99\\ 0.95\\ 0.95\\ 0.95\\ 0.99\\ 0.95\\ 0.95\\ 0.95\\ 0.99\\ 0.95\\$	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table C ₁ 17.8366 29.9479 56.0273 312.7813 11.7589 20.3032 37.2942 185.8586 12.2252 21.6253 42.9662 210.2504 10.6662 20.7545 38.9539	$\begin{array}{c} 2.4295\\ 4.7080\\ 15.8642\\ 1.3268\\ 1.9019\\ 3.1270\\ 15.3322\\ 1.4012\\ 2.1094\\ 4.4406\\ 19.0963\\ 1.3629\\ 2.1455\\ 3.8966\\ 16.3336\\ \hline \ \ $	$\begin{array}{c} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{maller EMSE}\\ \hline v = 1 \ \text{and} \ p=9\\ \hline \hline compse\\ \hline c_3\\ \hline 3.5982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ 2.6393\\ 5.1755\\ 9.2920\\ \hline \end{array}$	$\begin{array}{c} 1.5920\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \end{array}$
100 150 200 <u>n</u> 50 100 150 200	$\begin{array}{c} 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.99\\ 0.8\\ 0.9\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0.95\\ 0$	12.1742 20.1100 44.9510 189.7279 7.9619 15.27 27.2705 131.5003 8.9205 14.1834 30.6178 157.0304 7.6837 15.4263 28.4487 143.018	19.8980 44.4881 188.2678 7.9266 15.1989 27.1466 131.0075 8.8954 14.1451 30.5325 156.641 7.6684 15.3952 28.3901 142.7522 B Table 	2.4295 4.7080 15.8642 1.3268 1.9019 3.1270 15.3322 1.4012 2.1094 4.4406 19.0963 1.3629 2.1455 3.8966 16.3336 old indicated the sn 2 9: EMSEs for 1 c_2 1.6494 2.8947 3.8033 26.6251 1.3819 2.2728 3.2184 14.221 1.6152 2.4081 4.2817 16.1405 1.4143 2.4984 3.8493 19.4800	$\begin{array}{r} 4.8852\\ 11.5664\\ 45.5422\\ 2.1726\\ 3.9662\\ 6.6739\\ 35.2562\\ 2.4713\\ 3.8912\\ 8.6451\\ 42.8419\\ 2.2028\\ 4.5035\\ 7.9984\\ 39.3749\\ \text{naller EMSE}\\ \textbf{v} = 1 \text{ and } p=9\\ \hline \textbf{COMPSE}\\ \hline \textbf{c}_3\\ \hline \textbf{cOMPSE}\\ \hline \textbf{c}_3\\ \hline \textbf{c}_35982\\ 6.4574\\ 11.2609\\ 69.7525\\ 2.6686\\ 4.7265\\ 7.9611\\ 38.9949\\ 3.0121\\ 4.9657\\ 10.0226\\ 47.3655\\ 2.6393\\ 5.1755\\ 9.2920\\ 49.0255\\ \hline \end{array}$	$\begin{array}{c} 1.5920\\ 11.5920\\ 43.5135\\ 2.1689\\ 4.0940\\ 6.1911\\ 36.1952\\ 2.4747\\ 3.9483\\ 8.6224\\ 43.4421\\ 2.3043\\ 5.0588\\ 8.1217\\ 41.3574\\ \hline \end{array}$	$\begin{array}{c} 2.4120\\ 4.6714\\ 15.7598\\ 1.3240\\ 1.8964\\ 3.1166\\ 15.2779\\ 1.3993\\ 2.1058\\ 4.4303\\ 19.0511\\ 1.3616\\ 2.1426\\ 3.8902\\ 16.3061\\ \hline \end{array}$	$\begin{array}{c} & .1763\\ 13.3608\\ 46.8489\\ 2.9569\\ 5.3999\\ 8.7935\\ 42.0009\\ 3.3992\\ 5.2536\\ 11.1534\\ 56.3899\\ 3.1764\\ 6.1252\\ 10.5169\\ 51.0804\\ \end{array}$

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Table 10: EMSEs for $\nu = 1.25$ and $p=9$									
2				COMPSE	-				
ρ^2	MLE	<i>C</i> ₁	<i>C</i> ₂	<i>C</i> ₃	C_4	C ₅			
0.8	29.8120	28.5768	2.1102	4.9335	3.9226	2.0495			
0.9	50.7526	48.7797	3.0771	8.8107	7.1843	2.9813			
0.95	100.4128	97.1939	4.7484	16.3670	11.1816	4.6287			
0.99	519.9196	508.1721	29.7907	94.2948	70.3630	29.2287			
0.8	16.2607	15.9571	1.3567	2.8967	2.5253	1.3465			
0.9	28.8359	28.2972	2.0835	4.9465	3.8663	2.0596			
0.95	62.6879	61.5431	4.0800	11.3018	8.7442	4.0185			
0.99	270.8632	267.4712	14.0441	45.1085	30.6100	13.8882			
0.8	18.4796	18.2584	1.6304	3.4844	2.8335	1.6202			
0.9	31.2447	30.8644	2.3371	5.6250	4.3683	2.3175			
0.95	70.0785	69.2906	4.5931	13.0057	9.7575	4.5503			
0.99	317.0939	314.1604	23.3084	62.8/03	51.9734	23.1080			
0.8	17.3403	17.1807	1.6261	3.3/96	2.9540	1.6183			
0.9	35.0910	34.7739	2.6425	6.9631	0.3790	2.6259			
0.95	59.5165 200 90F	58.9942	4.4078	11.3089	9.3730	4.3//5			
0.99	309.803	307.907	19.1049 Rold indicated the s	maller EMSE	40.9094	19.0455			
			bolu mulcateu tile s	maner EMSE					
		Table 1	11: EMSEs for <i>v</i>	= 0.85 and $p=2$	12				
o^2				COMPSE					
μ	MLE	<i>c</i> ₁	<i>C</i> ₂	<i>C</i> ₃	C ₄	C ₅			
0.8	30.2268	29.8619	2.0519	5.7249	4.8988	2.0369			
0.9	55.9570	55.3580	5.0961	11.8682	11.5056	5.0562			
0.95	130.3971	129.061	11.1001	30.1568	28.5111	11.0038			
0.99	530.9519	527.7231	36.4428	107.1048	102.876	36.2200			
0.8	11.6471	11.5917	1.4046	2.6799	2.7015	1.4014			
0.9	21.8890	21.7877	2.4383	5.0299	4.7187	2.4306			
0.95	43.0677	42.8641	3.8081	9.3312	8.7583	3.7942			
0.99	217.66	216.93	18.5146	50.4187	53.1009	18.4600			
0.8	11.6/00	11.6357	1.6905	3.1125	3.3012	1.6876			
0.9	20.1339	20.0777	2.2421	4.9004	4.9984	4.1250			
0.95	41.8139	41.0944	4.1334	9.7494	9.8302	4.1239			
0.99	0 2004	0 2002	1 22/1	2 2564	22524	1/.40/9			
0.8	9.3094	9.2902	2 0270	4 5572	2.3324 4 7EE1	2.0245			
0.9	34.6227	34.5528	2.0370	4.5575 8.284A	4.7551 8.4306	2.0345			
0.99	156 448	156 193	15 5181	38 1152	38 2063	15 4951			
0.77	100.110	100.170	Bold indicated the s	maller EMSE	50.2005	1011701			
		Table	12: EMSES for	$v = 1$ and $p = 1_2$	2				
ρ^2 ·	MLE		-	COMPSE	-				
0.0	MLE 40 5024		C ₂	C ₃	C ₄	<i>C</i> ₅			
0.8	48.5934	47.4954	3.3632	8./121	8.2088	3.3029			
0.9	//.4855	147 0000	4.4445	13.41/1	20.0445	4.3011			
0.93	130.371	147.9909	0.2944	20.4704	175 / 100	0.1040			
0.99	16 1166	16 2000	47.0374	2 4025	2 1007	47.1092			
0.0	33 5598	33 2668	2 4 3 3 9	6 5 8 6 2	6.0150	2 4102			
0.95	62.0426	61.5142	4.5741	12.1235	10.3679	4.5423			
0.99	318,6942	316.7213	17.0613	57.4023	47,2060	16.9632			
0.8	15.8929	15.8042	1.4558	3.2192	3.0713	1.4521			
0.9	27.6453	27.4919	2.3008	5.3943	4.8452	2.2922			
0.95	55.3014	54.9955	3.9494	10.5169	8.3756	3.9326			
0.99	277.5442	276.3905	20.3704	55.6302	46.0304	20,2893			
0.8	14.2363	14.1776	1.3940	2.9350	2.8181	1.3915			
0.9	25.0326	24.9315	2.1893	5.0682	4.3449	2.1836			
0.95	49.4963	49.2973	4.0990	10.3963	9.4561	4.0858			
0.99	247.9527	247.1612	18.4930	52.1994	49.0265	18.4388			
			Bold indicated the s	maller EMSE					

*c*₆ 5.1110 8.9824 14.7239

83.3667 3.0929 4.9256

11.0719 41.0175

41.0175 4.0118 5.7047 13.7462 61.9871

3.9643 7.9898

11.2819 65.999

с₆ 7.4582

14.1663 37.4655 120.1458 3.7111

6.9067 12.7959 66.7717

4.4215 7.0077 14.1508 57.3847 3.5667

3.5667 6.5408 11.7178 54.4191

*c*₆ 10.1686

15.7877 30.9811

30.9811 150.6116 4.3053 8.5112

 $\begin{array}{c} 13.8004 \\ 68.0070 \end{array}$

4.5957 7.096 13.9478 70.2910 4.0668

6.8289 13.5885 67.0262

п

50

100

150

200

п

50

100

150

200

п

50

100

150

200

Table 13: EMSEs for v = 1.25 and p=12

22	o ²	compse						
п	Ρ	MLE	C_1	<i>C</i> ₂	<i>C</i> ₃	c_4	C ₅	C ₆
50	0.8	66.5138	64.0073	3.0372	9.7563	7.0821	2.9489	10.2700
	0.9	114.975	110.9237	6.1130	18.2827	14.9224	5.9085	16.9588
	0.95	225.1859	219.2014	8.7937	32.8742	22.2083	8.5763	28.9148
	0.99	1220.882	1201.324	46.8510	180.4798	139.0976	46.1052	146.2542
100	0.8	23.8395	23.4027	1.4939	3.4445	2.6202	1.4816	3.8261
	0.9	47.6500	46.7618	2.7865	7.4517	5.9284	2.7503	7.9167
	0.95	93.3668	91.8145	4.5054	14.0700	10.4409	4.4413	14.7955
	0.99	485.9481	481.4397	17.6006	73.2696	51.4461	17.4287	80.1791
150	0.8	22.8557	22.5772	1.3937	3.3526	2.6201	1.3870	3.9435
	0.9	42.4388	41.9304	2.2662	6.5493	4.9716	2.2484	7.7202
	0.95	87.6691	86.7035	4.3972	13.8002	9.6368	4.3614	15.7909
	0.99	394.6527	391.5111	19.5328	62.4182	49.1158	19.3725	67.6536
200	0.8	20.6514	20.4682	1.5539	3.4525	2.8835	1.5474	4.3300
	0.9	38.2561	37.9073	2.3842	6.4367	5.2434	2.3707	7.6864
	0.95	71.4081	70.7905	3.8656	11.0292	8.2573	3.8390	12.2316
	0.99	358.3625	355.8587	17.0435	58.2462	45.1041	16.9289	62.7291

Bold indicated the smaller EMSE

Table 14: Estimated COM Poisson regression coefficients and MSEs for plastic plywood data

Terms MLE -	MIE						
	<i>C</i> ₁	<i>C</i> ₂	<i>c</i> ₃	c_4	C5	C ₆	
Constant	1.4397	1.4393	0.5670	0.8577	1.2232	0.5668	0.4532
x_1	0.4937	0.4936	0.1944	0.2941	0.4195	0.1944	0.1554
x_2	0.6011	0.6009	0.2367	0.3581	0.5107	0.2367	0.1892
<i>x</i> ₃	0.3818	0.3817	0.1504	0.2275	0.3244	0.1503	0.1202
x_4	0.7401	0.7399	0.2915	0.4409	0.6288	0.2914	0.2330
MSE	6.7689	4.9352	3.5339	3.1553	5.3734	2.3767	2.3100

With a fixed sample size, explanatory variables, and dispersion parameter, the EMSEs of the COMPSE, using all proposed Stein parameters, were lower than those of the MLE. When the model included correlated regressors, the EMSE decreased sample size increased. Additionally, the as multicollinearity and the number of regressors directly affected the performance of the estimators. The EMSEs were lowest for overdispersion compared to underdispersion and equidispersion. Therefore, based on simulation and real application results, we conclude that our newly proposed estimator for the COMPRM is more appropriate than the MLE in the presence of multicollinearity and dispersion.

Compliance with ethical standards

Conflict of interest

The author(s) declared no potential conflicts of interest with respect to the research, authorship, and/or publication of this article.

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